Constructed Wetland

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TREATMENT WETLANDS

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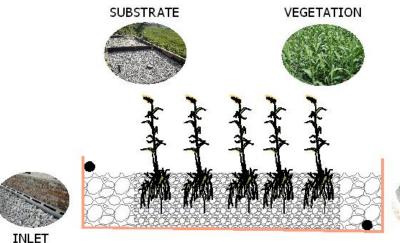




What is a Constructed Wetland?

- Engineered system designed to mimic/optimize processes found in natural wetland ecosystems;
- System that utilize wetland plants, soils and their associated microorganisms to remove contaminants from wastewater, as well as other sources of contamination.
- Biological wastewater treatment technology;











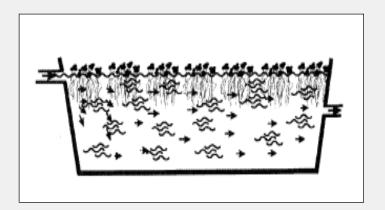
Classification/Types of CW

- Life form of the dominating macrophytes
- Flow pattern in the wetland systems
- Type of configurations of the wetland cells (hybrid systems, one-stage, multistage systems),
- Type of wastewater to be treated (industrial, municipal, grey water etc.),
- Treatment level of wastewater (primary, secondary or tertiary),
- Type of substrate (gravel, soil, sand, etc.), and
- Type of loading (continuous or intermittent loading).

Based on dominant macrophyte

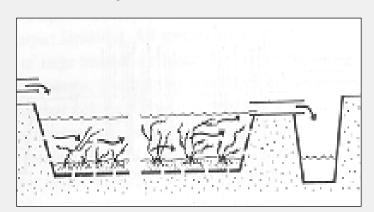


Free floating macrophytebased system



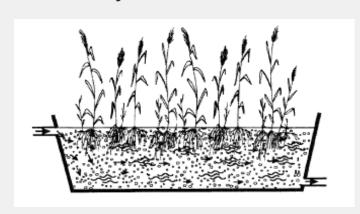


Submerged macrophytebased system



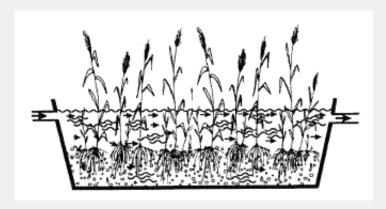


Emergent macrophytebased system



Based on flow pattern

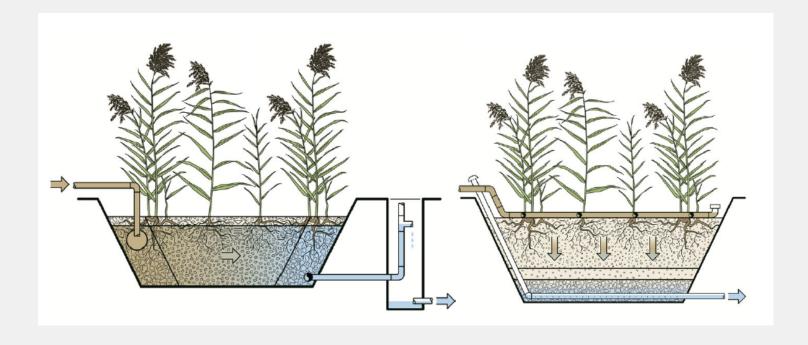
Free Water Surface (FWS) wetlands – majority of water flows above the soil surface





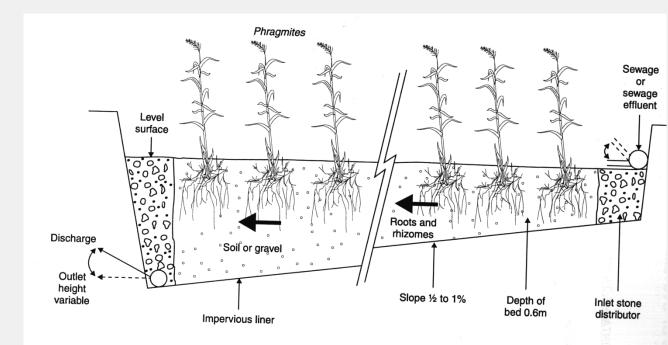
Sub Surface Flow (SSF) wetlands – flow is directed through the rooting media with no overland flow

- Horizontal Flow (HF)
- Vertical Flow (VF)



Horizontal Flow

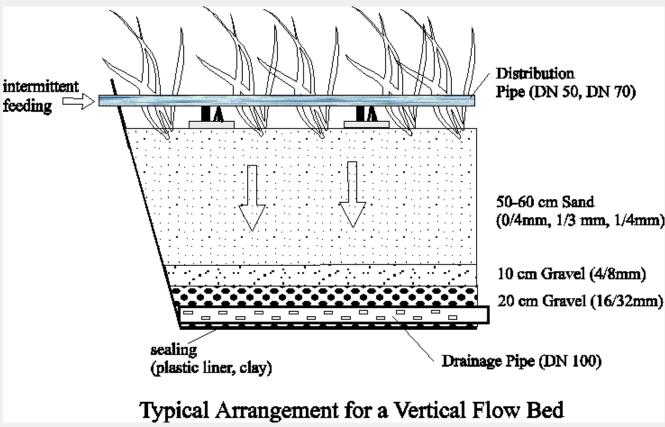
- Wastewater flows horizontally through a sand or gravel based filter whereby the water level is kept below the surface.
- Due to the water-saturated condition mainly anaerobic degradation processes occur.
- Effective primary treatment is required to remove particulate matter to prevent clogging of the filter.
- Emergent plants (macrophytes) are used.
- Are used for secondary or tertiary treatment.





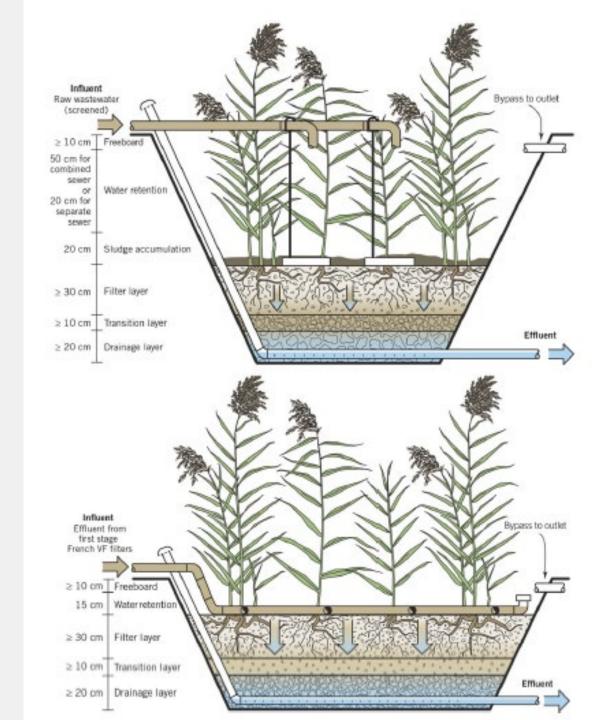
Vertical Flow

- Wastewater is intermittently loaded on the surface of the filter and percolates vertically through the filter.
- Between two loadings air re-enters the pores and aerates the filter so that mainly aerobic degradation processes occur.
- Effective primary treatment is required to remove particulate matter to prevent clogging of the filter.
- Emergent macrophytes are used.



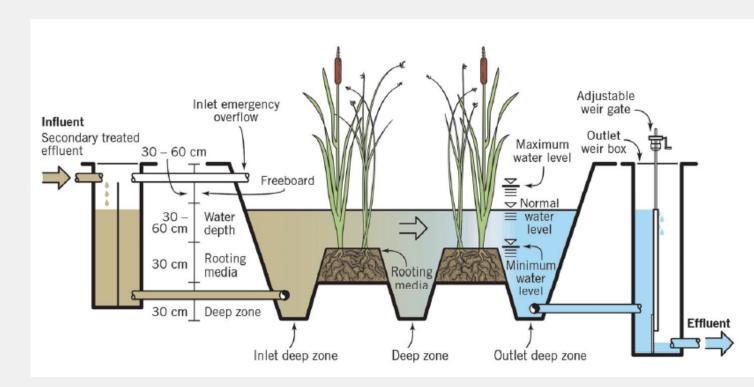
French Vertical Flow

- Are VF wetlands for treating screened wastewater.
- Two stages of wetlands operate in series and in parallel.
- Provide integrated sludge and wastewater treatment in a single step.
- No primary treatment unit is required.



Free Water Surface (FWS)

- Resemble natural wetlands in appearance.
- Require large surface area, are generally lightly loaded.
- Various plant genus can be used: a) emergent (b) submerged (c) floating: Eichornia (water hyacinth), Lemna (duckweed).
- Are mainly used for tertiary treatment.



Wetland plants



Typha or cattail



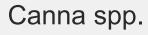
Phragmites or reed



Scirpus or bulrush

Wetland plants (flowering)







Iris spp.



Heliconia spp.

Typical removal efficiencies

Parameters	HF	VF a	French VF	FWS
Treatment step	Secondary	Secondary	Combined	Tertiary
(main application)			primary and	
			secondary	
Total Suspended Solids	> 80%	> 90%	> 90%	> 80%
Organic matter	> 80%	> 90%	> 90%	> 80%
(measured as oxygen				
demand)				
Ammonia nitrogen	20 - 30%	> 90%	> 90%	> 80%
Total nitrogen	30 - 50%	< 20%	< 20%	30 - 50%
Total phosphorus	10 - 20%	10 - 20%	10 - 20%	10 - 20%
(long term)				
Coliforms	2 log ₁₀	2 – 4 log ₁₀	1 – 3 log ₁₀	1 log ₁₀
a Single-stage VF bed, main layer of sand (grain size 0.06 – 4 mm)				

Single-stage vr ded, main layer of sand (grain size 0.00 – 4 min)

Land area requirement

Treatment technology	Treatment area requirement (m²/PE)
Facultative pond ^a	2.0 - 6.0
Anaerobic + facultative pond a	1.2 - 3.0
UASB reactor a	0.03 - 0.10
Activated sludge, SBR a	0.12 - 0.30
Trickling filter a	0.15 - 0.40
HF wetlands ^b	3.0 - 10.0
VF wetlands ^b	1.2 - 5.0
French VF wetlands c	2.0 - 2.5

^a (von Sperling, 2007a)

^b for warm (Hoffmann *et al.*, 2011) and temperate climates (Kadlec and Wallace, 2009)

^c for temperate climates (Molle et al., 2005)

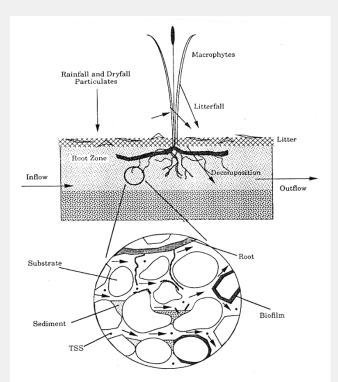
Pollutant and Pathogen removal mechanism

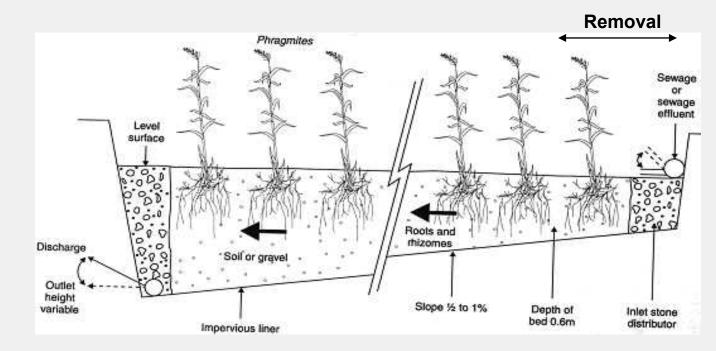
Parameter	Main removal mechanisms
Suspended solids	Sedimentation, filtration
Organic matter	Sedimentation and filtration for the removal of particulate organic matter, biological degradation (aerobic and/or anaerobic) for the removal of dissolved organic matter
Nitrogen	Ammonification and subsequent nitrification and denitrification, plant uptake and export through biomass harvesting
Phosphorus	Adsorption-precipitation reactions driven by filter media properties, plant uptake and export through biomass harvesting
Pathogens	Sedimentation, filtration, natural die-off, predation (carried out by protozoa and metazoa)

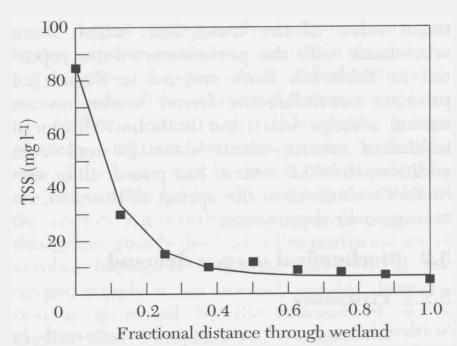
Suspended Solids

- Sedimentation
- Filtration

Most of the suspended solids are eliminated at the inlet end of the bed.





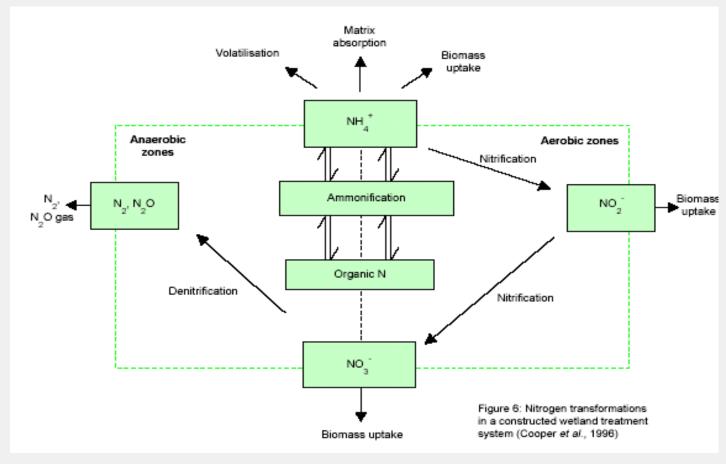


Organic matter

- Particulate organic matter
 - Filtration
 - Sedimentation
- Soluble organic matter (chemical reaction electrons are transferred from organic matter (electron acceptor) to a compound (electron donor) releasing energy for cell growth
 - Aerobic microbial respiration (oxygen is electron acceptor)
 CO₂ ★
 - Denitrification (nitrate and nitrite as electron acceptor) $N_2 + CO_2$
 - Sulphate reduction (sulphate as electron acceptor)
 S + CO₂ ★
 - Methanogenesis (organic matter is simultaneously electron acceptor and donor) CH₄ + CO₂ ★

Nitrogen

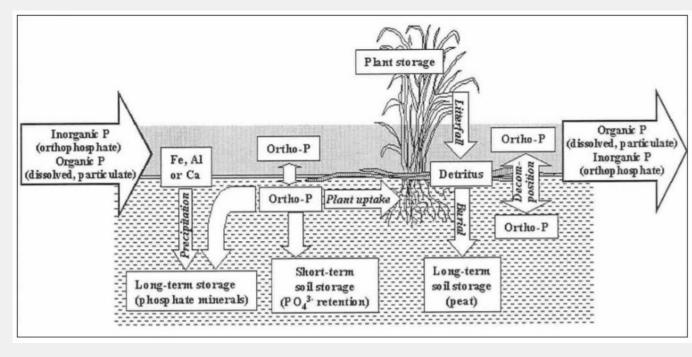
- Primary and Secondary Organic N and ammonium (NH₄-N) + nitrate (in tertiary systems)
 - Ammonification (organic N to ammonium)
 - Nitrification (oxidation of ammonium to nitrate)
 - Denitrification (nitrate to nitrogen gas)
 - Sorption (ammonium as cation sorbed onto media particles; zeolite)
 - Plant uptake (if plants are not harvested, no nitrogen removal)



Plant species	Uptake (kg/ha/year)	
Phragmites	750 – 2,450	
Scripus	125 - 775	
Typha	111 – 2,630	

Phosphorus

- Primarily as organic phosphorus and orthophosphate;
- Organic phosphorus is converted to orthophosphate as part of organic matter degradation;
- Chemical precipitation (usually happening in FWS)
- Sedimentation (usually happening in FWS)
- Sorption (Reactive media materials rich in Ca, Fe and Al) – usually happening in VF and HF
- Plant and microbial uptake



Pathogens

- Physical filtration and sedimentation
- Chemical oxidation and adsorption to organic matter
- Biological oxygen release and bacterial activity in root zone (rhizosphere); aggregation and retention in biofilms; natural die-off; predation and competition for limiting nutrient or trace elements

Advantages

- simple construction (can be constructed with local materials)
- simple O/M,
- low energy maintenance,
- little excess sludge production,
- cost effectiveness (low construction and operation costs),
- increase in biodiversity,
- utilization of the harvested aquatic plants for a variety of purposes (biomass, biogas, animal feed, fertilizer, using stems for thatching, matting, fencing, etc.)

Disadvantages

- large area requirement,
- not appropriate for treating some wastewater with high concentrations of certain pollutants,
- surface flow wetlands can attract mosquitoes and other pests,
- performance of wetlands may vary based on usage and climatic conditions,
- there may be a prolonged initial start-up period before vegetation is adequately established

Design approaches

- HF and FWS CW
 - Loading charts
 - Plug-flow k-C*
 - P-k-C*

- VF and French VF CW
 - Rule of thumb (also used for HF CW)

Rule of thumb

- Based on a particular CW application in a specific climate or geographical region;
- Local or national guideline for a single CW technology

Country	Technology	Specific surface area (m²/PE)	Reference	
Austria	VF	4	ÖNORM B 2505 (2009)	
Denmark	HF	5	Brix and Johansen (2004)	
	VF	3	- Dim and Johanson (2001)	
Germany	VF	4	DWA-A 262 (2017)	
France	French VF	2	Iwema et al. (2005)	

Plug-flow k-C* (first order equation)

$$A = \frac{Q_{\rm i}}{k_{\rm A}} \ln \left(\frac{C_{\rm o} - C^*}{C_{\rm i} - C^*} \right)$$

where:

 C_{\circ} = outlet concentration, mg/L

 C_i = inlet concentration, mg/L

 C^* = background concentration, mg/L

 $k_A =$ modified first-order areal rate coefficient, m/d

 $Q_i = \text{influent flow rate, m}^3/d$

$$k_{\rm T} = k_{20} \Theta^{(T-20)}$$

where:

 $k_{\rm T}$ = rate coefficient at water temperature T

 k_{20} = rate coefficient at water temperature 20°C

T =water temperature, °C

 θ = modified Arrhenius temperature factor, dimensionless

Example temperature correction factors (θ -values) for HF and FWS wetlands (50^{th} percentile values, Kadlec and Wallace, 2009).

Parameter	HF	FWS
BOD ₅	0.981	0.985
TN	1.005	1.056
NH ₄ -N	1.014	1.014
NO_x -N	_	1.102
Thermotolerant coliform	1.002	_

Mass loading charts

- From a collection of 1,500 small-scale wetlands around the world;
- Lines correspond to 50th, 75th and 90th percentile data collected;
- Based on influent mass loading rate, desired effluent concentration and risk tolerance.

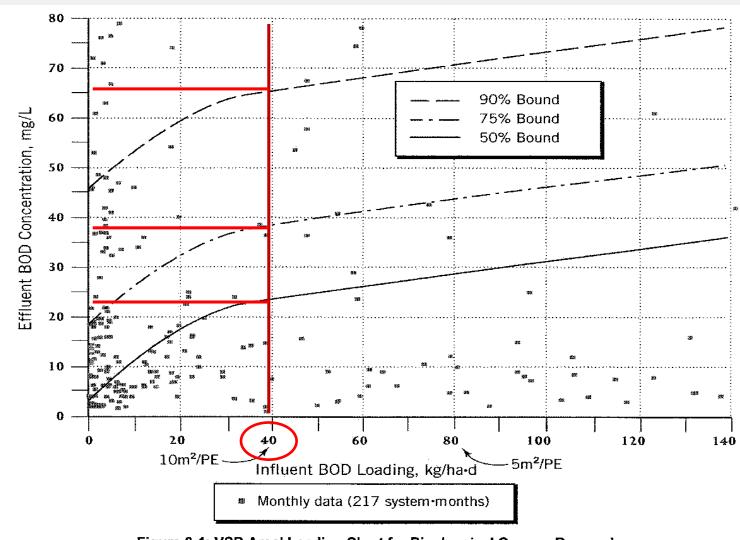
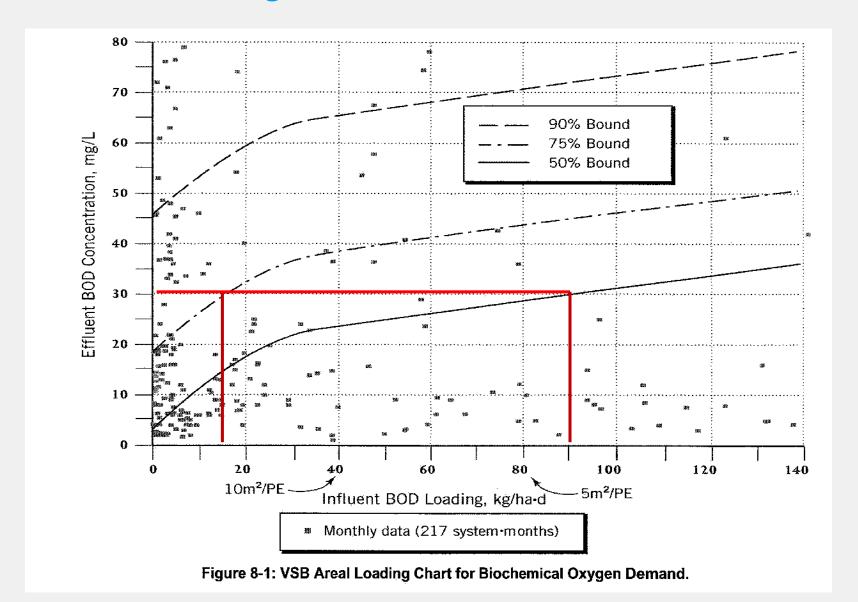
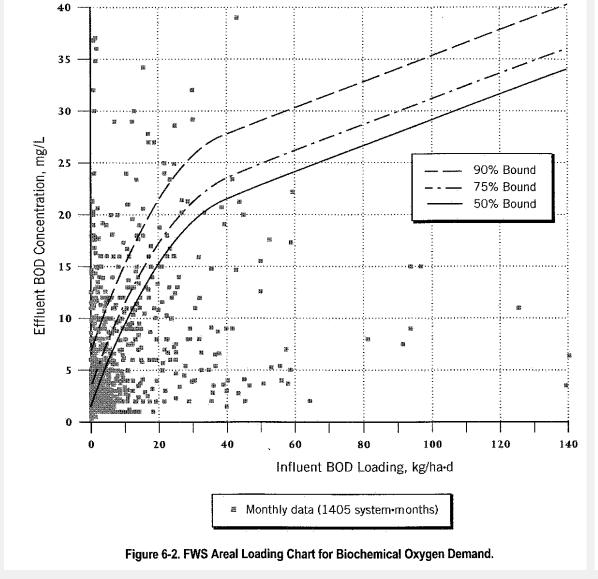


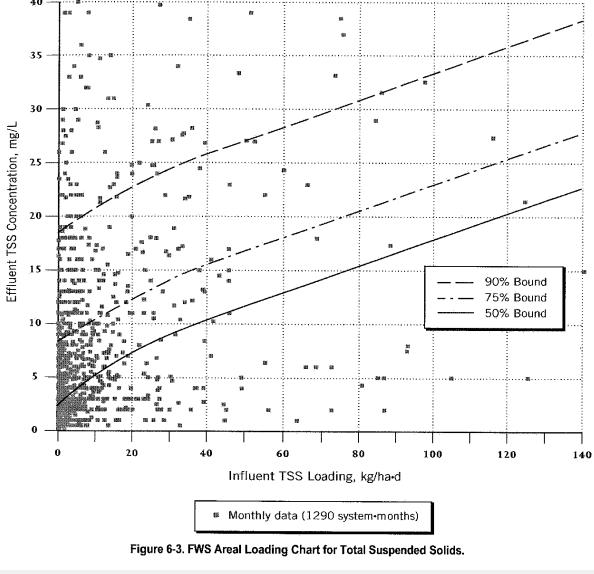
Figure 8-1: VSB Areal Loading Chart for Biochemical Oxygen Demand.

Mass loading charts

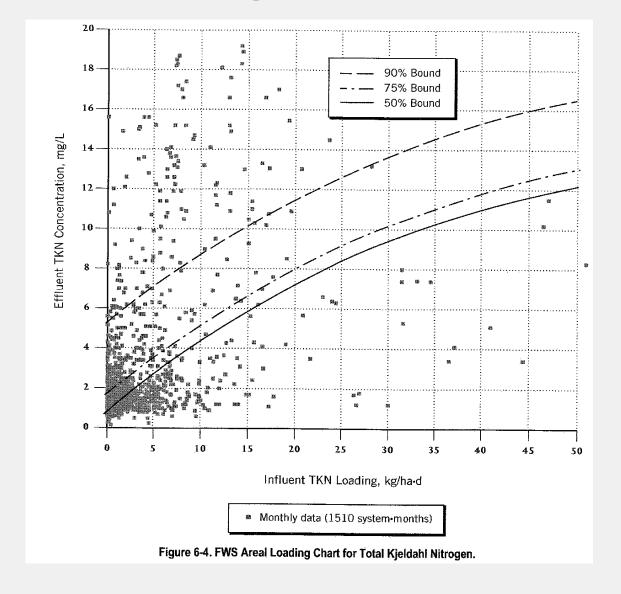


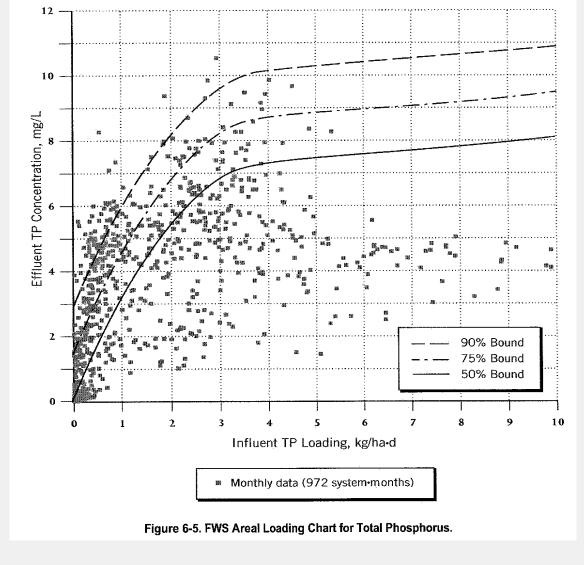
Mass loading chart for FWS





Mass loading chart for FWS





Mass loading chart for HF CW

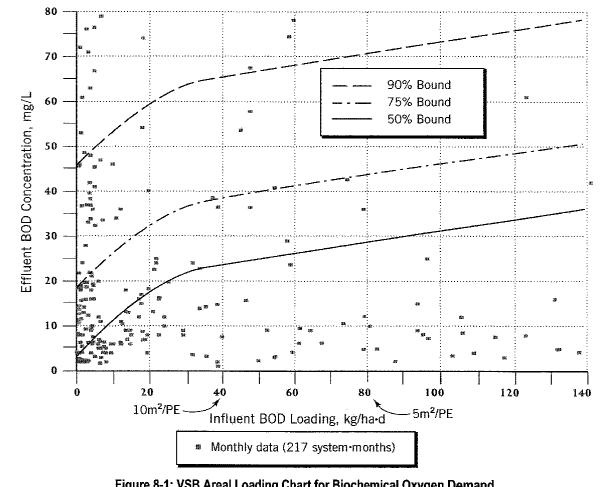
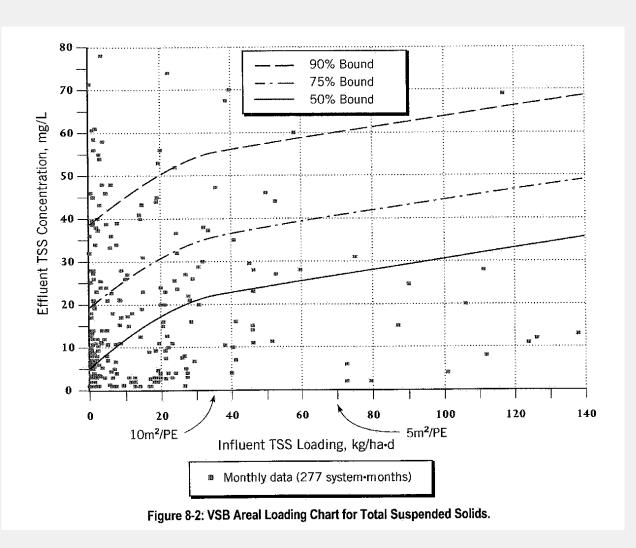


Figure 8-1: VSB Areal Loading Chart for Biochemical Oxygen Demand.



Mass loading chart for HF CW

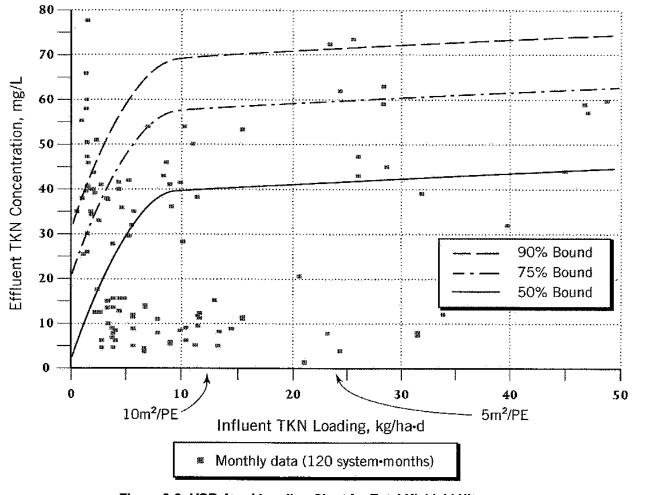


Figure 8-3: VSB Areal Loading Chart for Total Kjeldahl Nitrogen.

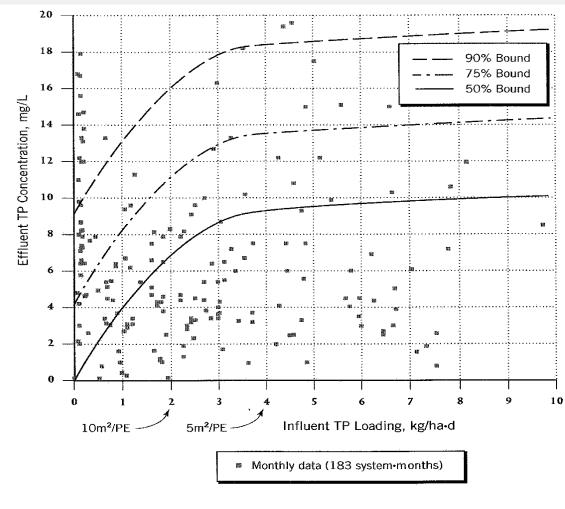


Figure 8-4. VSB Areal Loading Chart for Total Phosphorus.

Modified first order equation P-k-C*

$$A = \frac{PQ_i}{k_A} \left(\left(\frac{C_i - C^*}{C_o - C^*} \right)^{\frac{1}{p}} - 1 \right) = \frac{PQ_i}{k_V h} \left(\left(\frac{C_i - C^*}{C_o - C^*} \right)^{\frac{1}{p}} - 1 \right)$$

where:

 $C_o = \text{outlet concentration, mg/L}$

 C_i = inlet concentration, mg/L

 C^* = background concentration, mg/L

h = wetland water depth, m

 k_A = first-order areal rate coefficient, m/d

 $k_{\rm v}$ = first-order volumetric rate coefficient, 1/d

P = apparent number of tanks-in-series (TIS), dimensionless

 $Q_i = \text{influent flow rate, m}^3/d$

Modified first order equation P-k-C*

Examples of P values for HF, VF, and FWS wetlands (Kadlec and Wallace, 2009).

Parameter	HF	VF	FWS
BOD ₅	3	2	1
TN	6	n.g. a	3
NH ₄ -N	6	6	3

Example background concentrations (C*) in mg/L for HF, VF, and FWS wetlands (Kadlec and Wallace, 2009).

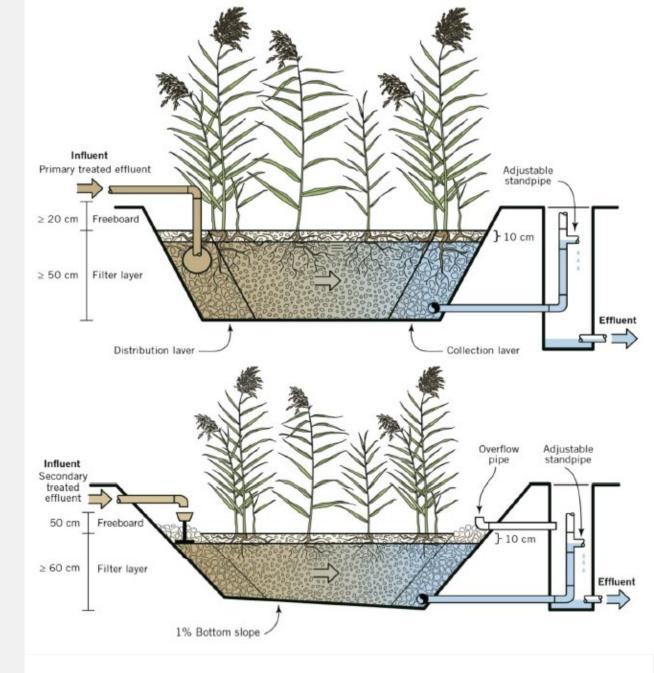
	HF VF		FV	FWS	
Parameter -			Lightly Loaded	Heavily Loaded	
BOD ₅	10	2	2	10	
TN	1	0	1.5		
NH ₄ -N	0	0	0.1	0.1	

Example areal-based reaction rate coefficients (50th percentile) for HF and FWS wetlands (Kadlec and Wallace, 2009).

Pollutant	HF k _A -rate (m/yr)	FWS k _A -rate (m/yr)
BOD ₅	25	33
TN	8.4	12.6
NH ₄ -N	11.4	14.7
NO _x -N	41.8	26.5
Thermotolerant coliform	103	83

Horizontal Flow CW

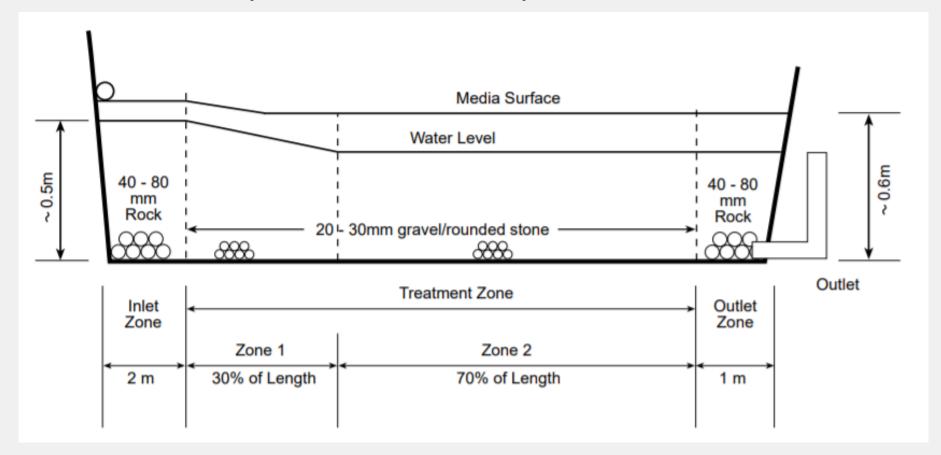
- Used for secondary and tertiary treatment (mostly in the UK);
- Primary treatment is mandatory (e.g. septic tank; ABR);
- Gravel bed is saturated and planted with emergent macrophytes;
- Bed is isolated from the surrounding (e.g. plastic liner; geotextile membrane);
- Gravel depth 0.5 to 0.7 m and water depth is 5-10 cm below the surface;



Typical schematic of a HF wetland; top: secondary treatment; bottom: tertiary treatment of domestic wastewater.

HF CW – Media and depth

Media and depth of a HF CW as per US-EPA



 Most frequently used media size in Europe/UK is 8-16 mm and have been built 0.6 m deep

Inlet (continuous loading)

• Pipes (perforated)







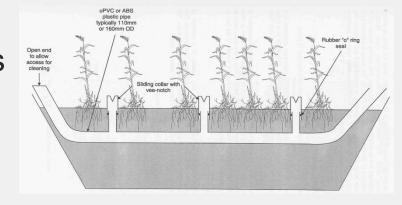




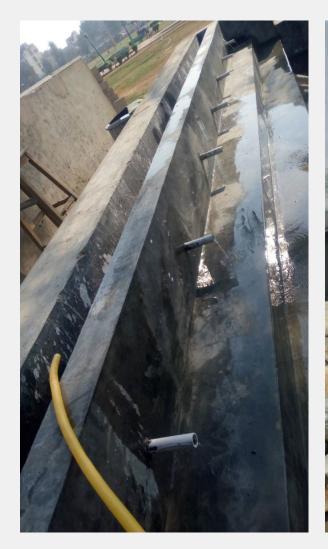


Channels

Riser pipes with vee-notches



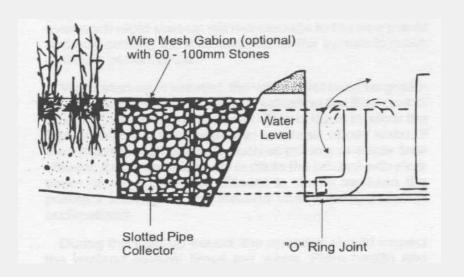
Inlet (continuous loading)



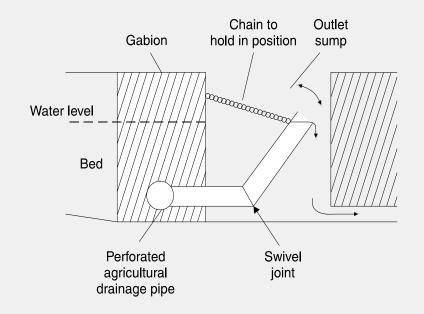


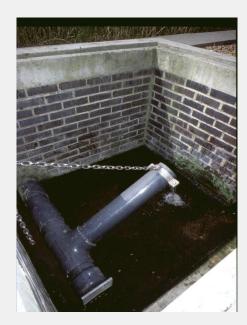
Outlet

Elbow outlet









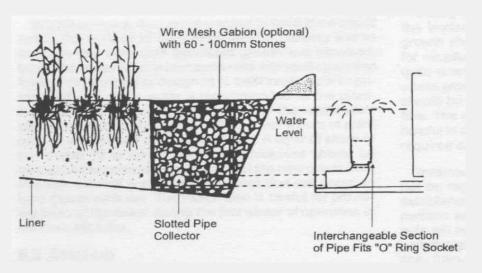
Outlet

held in place by rope or chain Water level

Flexible pipe

Flexible plastic pipe

Socketed pipe





Site clearance, earthwork in excavation



Compaction



Construction of wall/basin



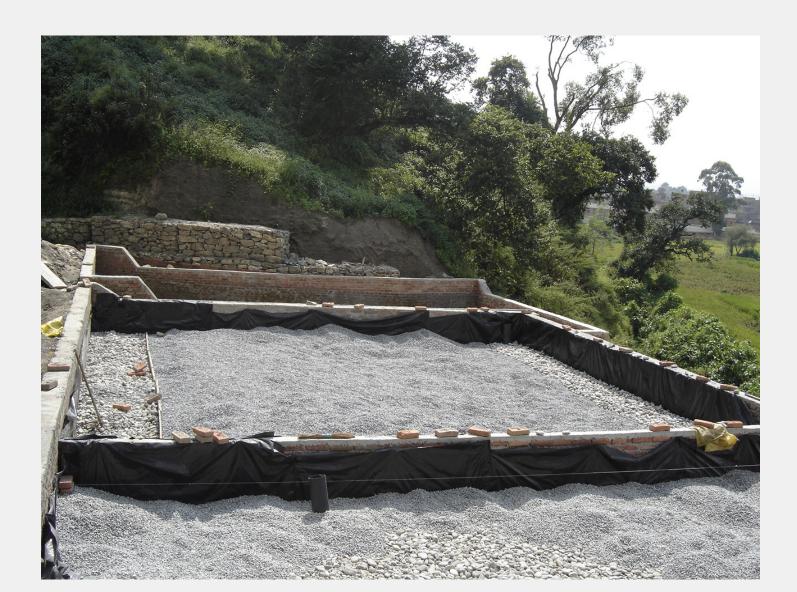
Basin ready for lining



Sealing/plastic liner



Filling of substrate



HF CW with plantation



HF CW in operation



Design

Design a HF CW for five households (20PE) for a small community in a temperate climate. The average per capita wastewater generation is 150L/day and BOD₅ load of 60g per person per day (DWA, 2017). The effluent from the HF CW should meet the BOD₅ effluent standard of 30 mg/L.

Assume that a primary treatment precedes the HF CW and reduces the BOD₅ load by 1/3.

Rule of thumb

Country	Technology	Specific surface area (m²/PE)	Reference	
Austria	VF	4	ÖNORM B 2505 (2009)	
Denmark	HF	5	Drive and Jahansan (2004)	
	VF	3	Brix and Johansen (2004)	
Germany	VF	4	DWA-A 262 (2017)	
France	French VF	2	Iwema et al. (2005)	

Area = $5 \times 20 = 100 \text{ m}^2$

Plug flow k-C*

$$A = \frac{Q_{\rm i}}{k_{\rm A}} \ln \left(\frac{C_{\rm o} - C^*}{C_{\rm i} - C^*} \right)$$

where:

 C_{\circ} = outlet concentration, mg/L

 $C_{\rm i}$ = inlet concentration, mg/L

 C^* = background concentration, mg/L

 $k_A =$ modified first-order areal rate coefficient, m/d

 $Q_i = \text{influent flow rate, m}^3/d$

Example background concentrations (C^*) in mg/L for HF, VF, and FWS wetlands (Kadlec and Wallace, 2009).

	HF	VF	FWS	
Parameter -			Lightly Loaded	Heavily Loaded
BOD_5	10	2	2	10
TN	1	0	1.5	
NH ₄ -N	0	0	0.1	0.1

Calculate Q_i

Average wastewater production = 150 Litres per capita per day

Number of users = 20

Qi = 20 X 150 = 3,000 Litres/day = 3 m³/day

Calculate C_i

Average BOD₅ production = 60 g per person per day

 BOD_5 concentration = $(60 \times 1,000)/150 = 400 \text{ mg/L}$

 BOD_5 removal in primary treatment = 1/3 (33%)

 BOD_5 inlet concentration = (2/3) X 400 = 266.66

mg/L

 $C_0 = 30 \text{ mg/L}$

Example areal-based reaction rate coefficients (50th percentile) for HF and FWS wetlands (Kadlec and Wallace, 2009).

FWS

HF

k_A (Table)

Pollutant	k _A -rate (m/yr)	k _A -rate (m/yr)
BOD ₅	25	33
TN	8.4	12.6
NH ₄ -N	11.4	14.7
NO _x -N	41.8	26.5
Thermotolerant coliform	103	83

 $Area = 111.78 \text{ m}^2$

Plug flow k-C* (dimensioning and check for design)

Dimension Length:Width rate (2:1 to 4:1)

Width of HF CW = 7 (assume)
Length of HF CW = Area/Depth =
111.78/7 = 15.97 m
Check for Length:Width ratio = 2.28:1

Provide length = 16 m Depth = 0.50 m Check for cross-sectional organic loading < 250 g BOD₅ / (m².d)

Cross-sectional area = $W \times D = 7 \times 0.5 = 3.5 \text{ m}^2$

BOD₅ load in (M_i) = BOD₅ concentration x Inflow Q

 $= 266.7 \times 3 = 800 \text{ g BOD}_5 / \text{d}$

Cross-sectional organic loading rate

= M_i/Cross-sectional area

 $= 800 / 3.5 = 228.57 \text{ g BOD}_5 / (\text{m}^2.\text{d})$

Modified Plug flow P-k-C*

$$A = \frac{PQ_{i}}{k_{A}} \left(\left(\frac{C_{i} - C^{*}}{C_{o} - C^{*}} \right)^{\frac{1}{p}} - 1 \right) = \frac{PQ_{i}}{k_{V}h} \left(\left(\frac{C_{i} - C^{*}}{C_{o} - C^{*}} \right)^{\frac{1}{p}} - 1 \right)$$

where:

 C_{\circ} = outlet concentration, mg/L

 C_i = inlet concentration, mg/L

 C^* = background concentration, mg/L

h = wetland water depth, m

 k_A = first-order areal rate coefficient, m/d

 k_v = first-order volumetric rate coefficient, 1/d

P =apparent number of tanks-in-series (TIS), dimensionless

 $Q_i = \text{influent flow rate, m}^3/d$

 $Q_i = 3 \text{ m}^3/\text{day}$

 $C_i = 266.66 \text{ mg/L}$

 $C^* = 10 \text{ mg/L}$

 $C_0 = 30 \text{ mg/L}$

 $k_A = 25 \text{ m/yr} = 0.068 \text{ m/d}$

P (From table)

Examples of *P* values for HF, VF, and FWS wetlands (Kadlec and Wallace, 2009).

Parameter	HF	VF	FWS
BOD ₅	3	2	1
TN	6	n.g. a	3
NH ₄ -N	6	6	3

n.g. = not given

Area = 176.24 m^2

Modified Plug flow k-C* (dimensioning and check for design)

Dimension Length:Width rate (2:1 to 4:1)

Width of HF CW = 9 (assume)
Length of HF CW = Area/Depth =
176.24/9 = 19.58 m
Check for Length:Width ratio = 2.18:1

Provide length = 20 m Depth = 0.50 m Check for cross-sectional organic loading < 250 g BOD₅ / (m².d)

Cross-sectional area = $W \times D = 9 \times 0.5 = 4.5 \text{ m}^2$

BOD₅ load in (M_i) = BOD₅ concentration x Inflow Q = 266.7 x 3 = 800 g BOD₅ /d

Cross-sectional organic loading rate = M_i/Cross-sectional area

 $= 800 / 4.5 = 177.78 \text{ g BOD}_5 / (\text{m}^2.\text{d})$

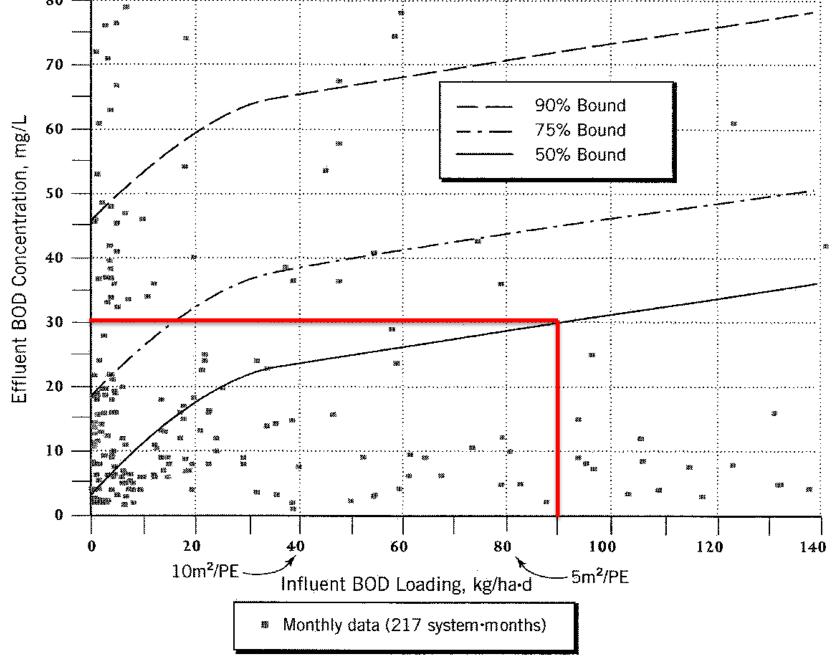


Figure 8-1: VSB Areal Loading Chart for Biochemical Oxygen Demand.

 BOD_5 load in (M_i) = 800 g BOD_5 /d

Choose confidence interval – 50% Effluent BOD₅ concentration = 30 mg/L

Influent BOD₅ loading rate

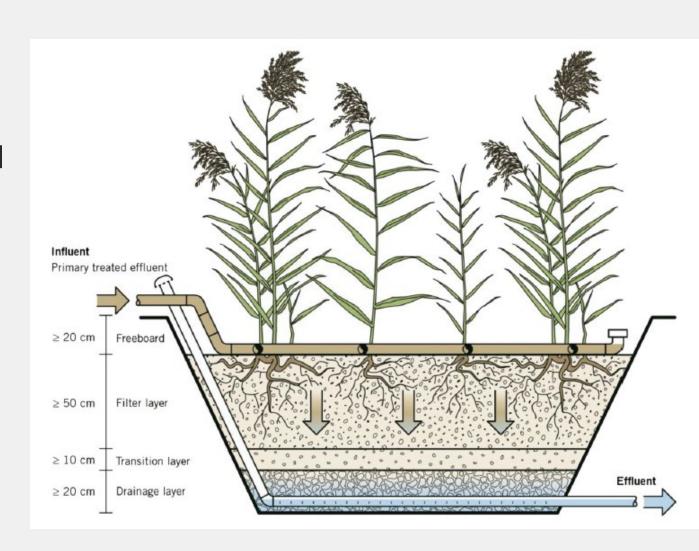
= 90 kg/ha-d

 $= 9 g/m^2-d$

Area = $800/9 = 88.89 \text{ m}^2$

Vertical Flow CW

- Secondary or tertiary wastewater treatment;
- Sand and/or gravel bed is planted with emergent macrophytes;
- Primary treated wastewater is loaded intermittently;
- Bed is isolated from the surrounding (e.g. plastic liner; geotextile membrane);
- Efficient for removal of organics and aerobic processes like nitrification;

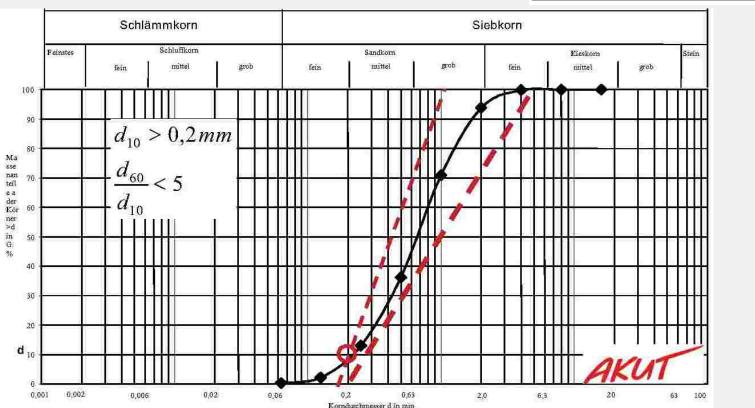


VF CW: Media & depth

Media

- Effective grain size $(d_{10}) > 0.2 \text{ mm}$
- Uniformity coefficient $(d_{60}/d_{10}) < 5$

Design Parameter	Denmark ^a	Germany	Austria
Main layer			
Filter material	Sand	Sand 0.06 – 2 mm	Sand 0.06 – 4 mm
Depth (cm)	100	> 50	> 50
d_{10} (mm)	0.25 - 1.2	0.2 - 0.4	0.2 - 0.4
$d_{60} (\mathrm{mm})$	1 - 4	-	-
$U = d_{60}/d_{10}$	< 3.5	< 5	-



transition layer (10 cm) - 4/8 mm drainage layer (20 cm) - 16/32 mm

Inlet (intermittent loading)







Outlet

 collection system of a network of perforated pipes surrounded by large stones at the bottom.





Substrate (main layer) filling in VF CW



Substrate (protection layer) filling in VF CW



Completed VF CW



Distribution network (intermittent loading)



VF CW in operation



Design

Design a VF CW for five households (20PE) for a small community in a temperate climate. The average per capita wastewater generation is 150L/day and BOD₅ load of 60g per person per day (DWA, 2017). The effluent from the VF CW should meet the BOD₅ effluent standard of 30 mg/L.

Assume that a primary treatment precedes the VF CW and reduces the BOD₅ load by 1/3.

Rule of thumb

Country	Technology	Specific surface area (m²/PE)	Reference	
Austria	VF	4	ÖNORM B 2505 (2009)	
Denmark	HF	5	Brix and Johansen (2004)	
	VF	3	- Dim and volkingen (2001)	
Germany	VF	4	DWA-A 262 (2017)	
France	French VF	2	Iwema et al. (2005)	

Area = $4 \times 20 = 80 \text{ m}^2$

Modified Plug flow P-k-C* (k_A – Cairo)

Table 6 The effect of different operational conditions of constructed wetland on the areal removal rate (k_A) and volumetric removal rate (k_V) of COD, BOD, TSS, NH₄ and TP.

Vegetation	Media type	COD	BOD	TSS	NH_4	TP
$\overline{k_V(d^{-I})}$						
Planted beds	Gravel	2.64 ^a	3.68 ^a	2.59 ^b	0.66^{b}	0.40^{b}
	Vermiculite	2.95 ^a	3.85 ^a	3.27^{a}	0.96^{a}	0.66^{a}
Unplanted beds	Gravel	0.76^{a}	0.98^{a}	1.04 ^a	0.52^{a}	0.24 ^b
•	Vermiculite	0.57 ^b	0.86 ^a	1.15 ^a	0.73 ^a	0.50^{a}
$k_A (m d^{-1})$						
Planted beds	Gravel	0.20	0.27	0.19	0.05	0.03
	Vermiculite	0.22	0.29	0.24	0.07	0.05
Unplanted beds	Gravel	0.06	0.07	0.08	0.04	0.02
•	Vermiculite	0.04	0.06	0.09	0.05	0.04

Values within the same column followed by the same superscript letter are not significantly different at P < 0.05.

Modified Plug flow P-k-C*

$$A = \frac{PQ_{i}}{k_{A}} \left(\left(\frac{C_{i} - C^{*}}{C_{o} - C^{*}} \right)^{\frac{1}{p}} - 1 \right) = \frac{PQ_{i}}{k_{V}h} \left(\left(\frac{C_{i} - C^{*}}{C_{o} - C^{*}} \right)^{\frac{1}{p}} - 1 \right)$$

where:

 C_{\circ} = outlet concentration, mg/L

 C_i = inlet concentration, mg/L

 C^* = background concentration, mg/L

h = wetland water depth, m

 k_A = first-order areal rate coefficient, m/d

 k_v = first-order volumetric rate coefficient, 1/d

P =apparent number of tanks-in-series (TIS), dimensionless

 $Q_i = \text{influent flow rate, m}^3/d$

 $Q_i = 3 \text{ m}^3/\text{day}$

 $C_i = 266.66 \text{ mg/L}$

 $C^* = 10 \text{ mg/L}$

 $C_o = 30 \text{ mg/L}$

 $k_A = 0.2 \text{ m/d}$

P (From table)

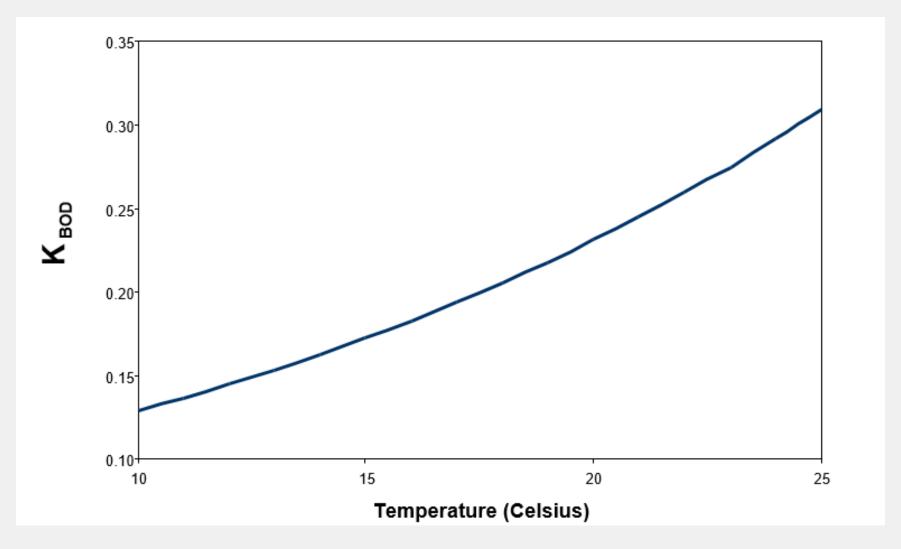
Examples of *P* values for HF, VF, and FWS wetlands (Kadlec and Wallace, 2009).

Parameter	HF	VF	FWS
BOD ₅	3	2	1
TN	6	n.g. a	3
NH ₄ -N	6	6	3

a n.g. = not given

Area = 77.47 m^2

Modified Plug flow P-k-C* (k_{BOD})







CONSTRUCTED WETLANDS MANUAL



Thank You!

Any Queries?

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